

Lawrence Livermore National Laboratory

Enhanced porosity and permeability in carbonate CO₂ storage reservoirs: An experimental and modeling study

Project Number: FWP-FEW0174 – Task 5

U.S. Department of Energy
National Energy Technology Laboratory
Carbon Storage R&D Project Review Meeting
Developing the Technologies and Building the
Infrastructure for CO₂ Storage
August 20-22, 2013



Presenter: Megan Smith
PI: Susan Carroll
Yue Hao

Presentation Outline

- Benefit to Program
- Project Overview
- Technical Status
- Accomplishments
- Summary
- Appendix



Benefit to the Program

- This research project quantifies relationships between fluid flow, heterogeneity, and reaction rates specific to carbon storage in carbonate reservoirs by integrating characterization, solution chemistry, and simulation data.
- This project meets the Carbon Storage Program goals to develop technologies that will support industries' ability to predict CO₂ storage capacity in geologic formations to within ± 30 percent.



Project Overview

Goals and Objectives

- The goal of this project is to calibrate key parameters in reactive transport models that will be used to predict final storage of CO₂ in carbonate EOR fields.
- This project will advance science-based forecasting for the transition of CO₂ – EOR operations to storage sites.
- Success is tied to the ability to scale reactive-flow and transport parameters over a range of carbonate rock types and permeability.



Technical Status

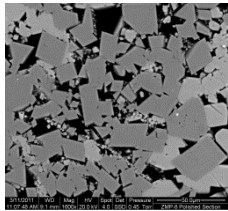
The research scope consists of three major tasks:

- Model calibration against existing experimental database of carbonate rocks from Midale-Weyburn Carbon Storage Project
 - Smith M, Sholokhova Y, Hao Y, and Carroll S, 2012, Evaporite caprock integrity: An experimental study of reactive mineralogy and pore-scale heterogeneity during brine–CO₂ exposure. *Env Sci & Technol*, doi:es3012723.
 - Carroll S, Hao Y, Smith M, Sholokhova Y, 2013, Development of scaling parameters to describe CO₂-carbonate-rock interactions for the Marly Dolostone and Vuggy Limestone, *Int J Greenhouse Gas Control*, doi:10.1016/j.ijggc.2012.12.026
 - Smith M, Sholokhova Y, Hao Y, and Carroll S. (2013) CO₂-Induced Dissolution of Low Permeability Carbonates Part I: Characterization and Experiments, *Adv Water Res*, revised.
 - Hao Y, Smith M, Sholokhova Y, and Carroll S. (2013) CO₂-Induced Dissolution of Low Permeability Carbonates Part 2: Numerical Modeling of Experiments, *Adv Water Res*, revised.
- **Study of a wider permeability range using cores from the Wellington, KS, CO₂ demonstration site (focus of presentation)**
- Refined model and parameter scaling towards predicting changes in reservoir porosity and permeability



Motivation behind choices of characterization techniques and experimental scales

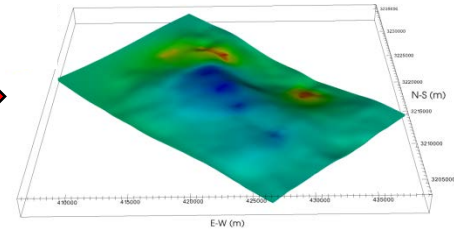
- ❑ Geochemical mineral-fluid interactions induced by CO₂ injection have a major effect on rock porosity and permeability evolution, which may potentially alter the behavior or performance of CO₂ geological storage and EOR operations;
- ❑ The mineral dissolution/precipitation and associated flow and reactive transport processes in porous media are described at different scales;



Pore (microscopic) scale ~ μm



Core (laboratory) scale ~ cm

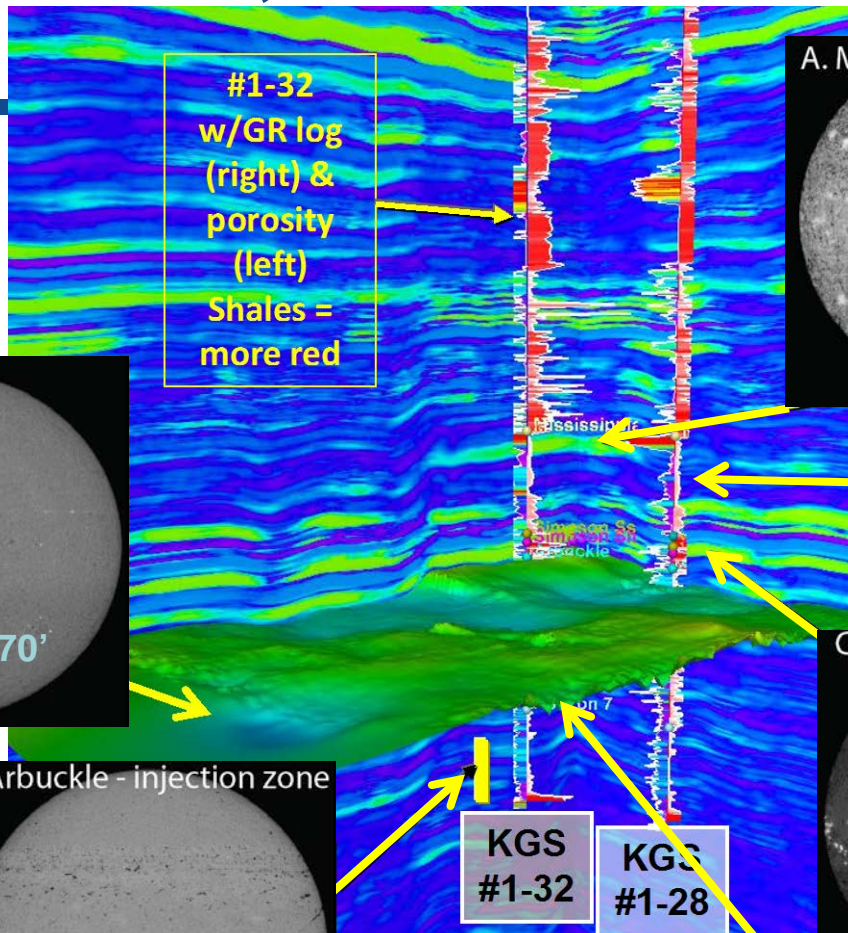


Large (reservoir/field) scale ~ km

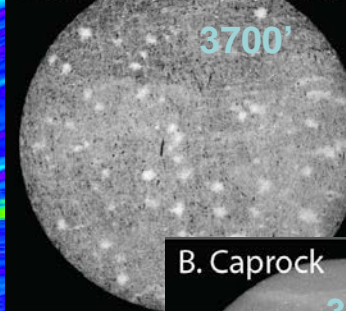
- ❑ Reactive transport modeling represents a critical component in assessment of geochemical impact of CO₂ water-rock interactions;
- ❑ **However, a lack of proper calibration or upscaling of the effective macroscopic parameters over large field-scales hinders accurate reactive-transport modeling of CO₂ fate and transport.**



Wellington, Kansas, flow unit model & samples



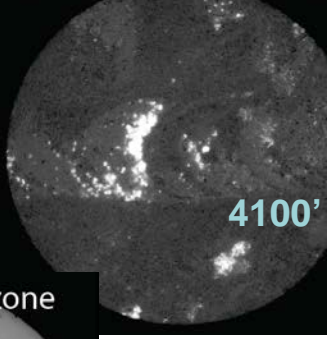
A. Mississippian pay zone



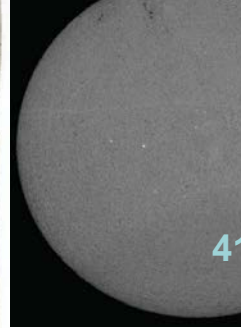
B. Caprock



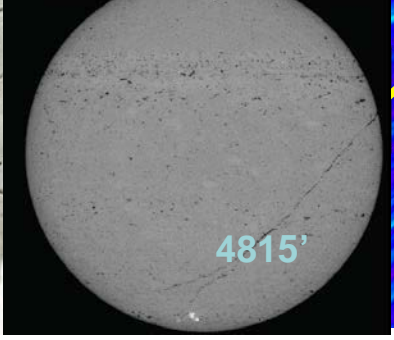
C. Simpson Sandstone



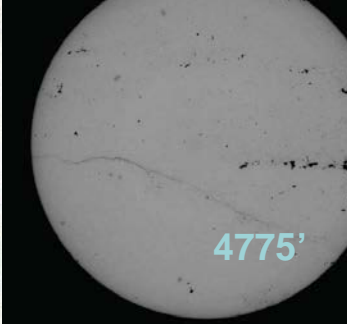
D. Arbuckle - top



F. Arbuckle - injection zone



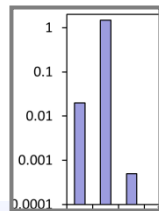
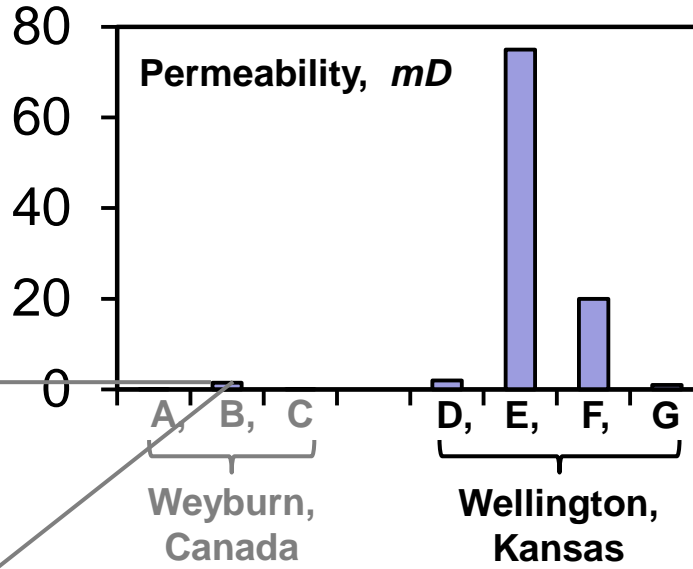
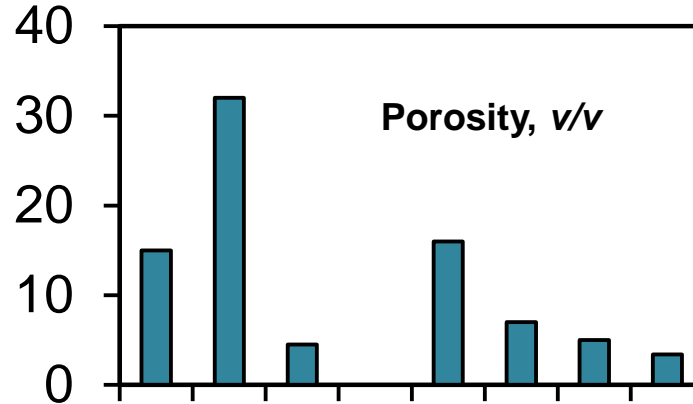
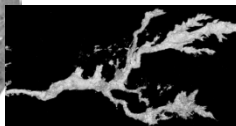
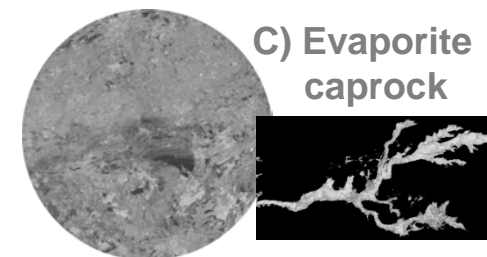
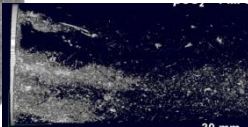
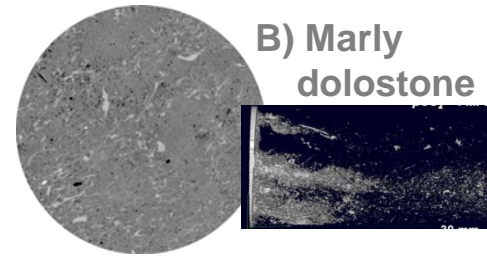
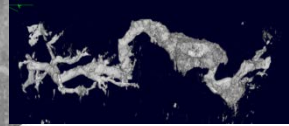
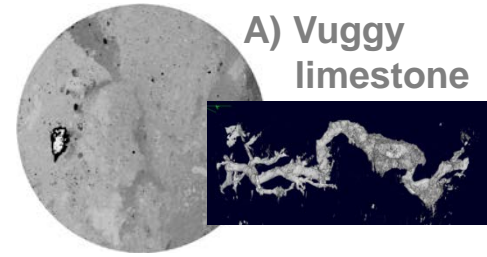
E. Arbuckle - baffle zone



*model image, cores
courtesy of KGS*

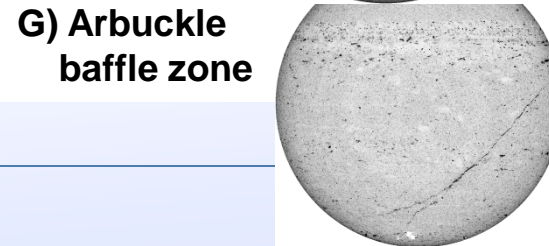
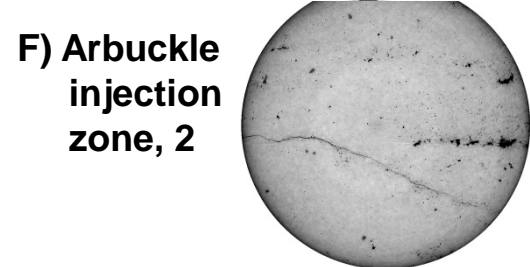
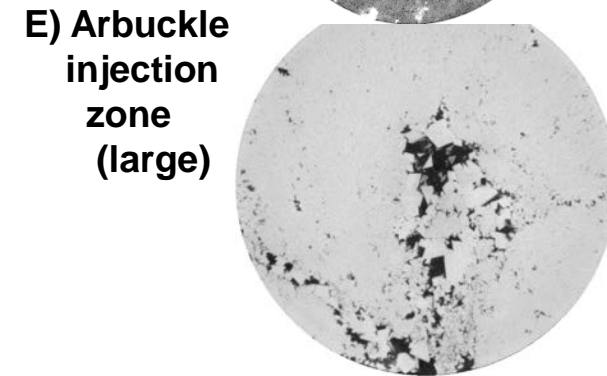


Wellington, KS, samples extend permeability range

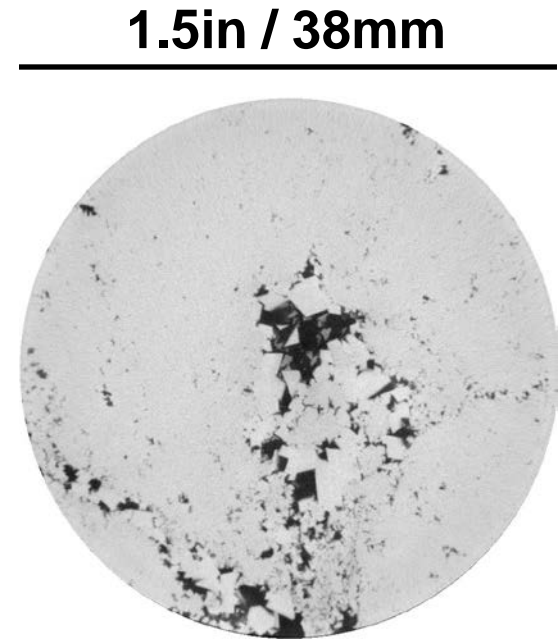
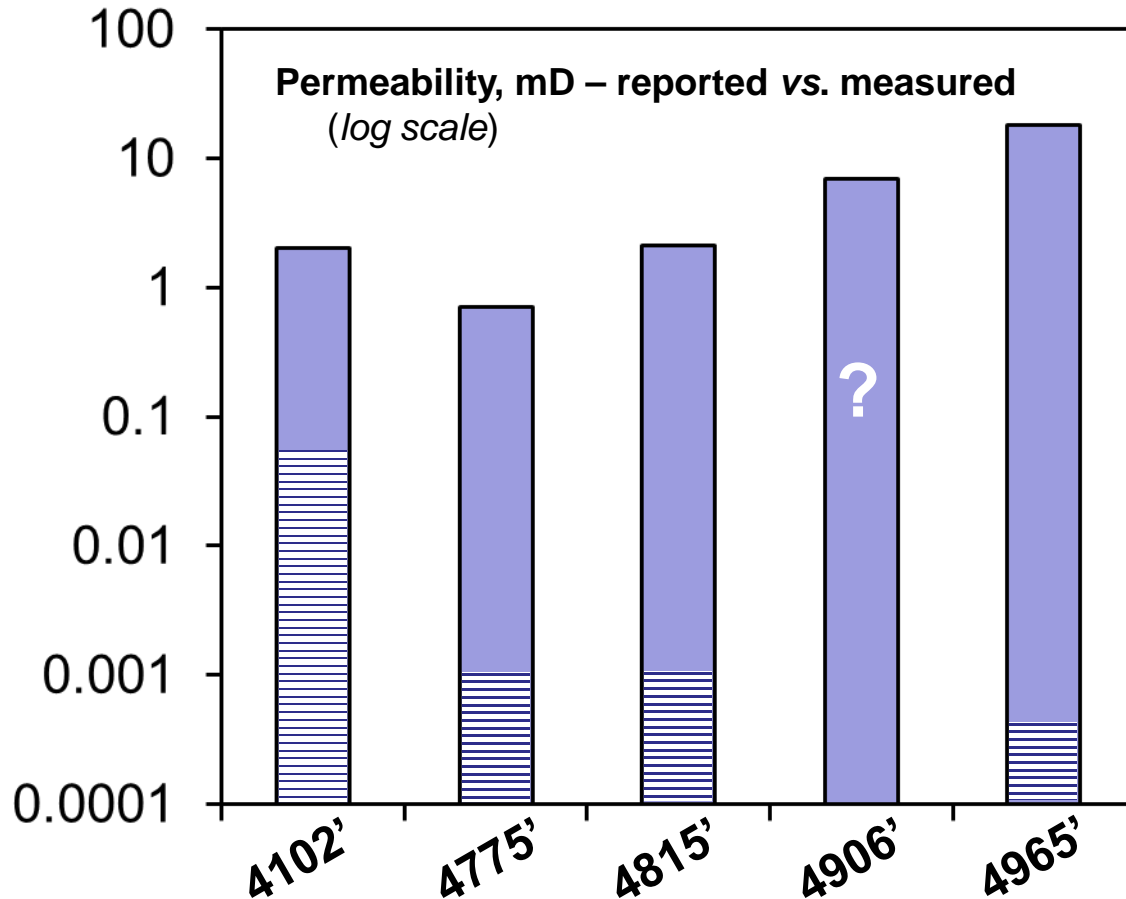


Weyburn, Canada

Wellington, Kansas



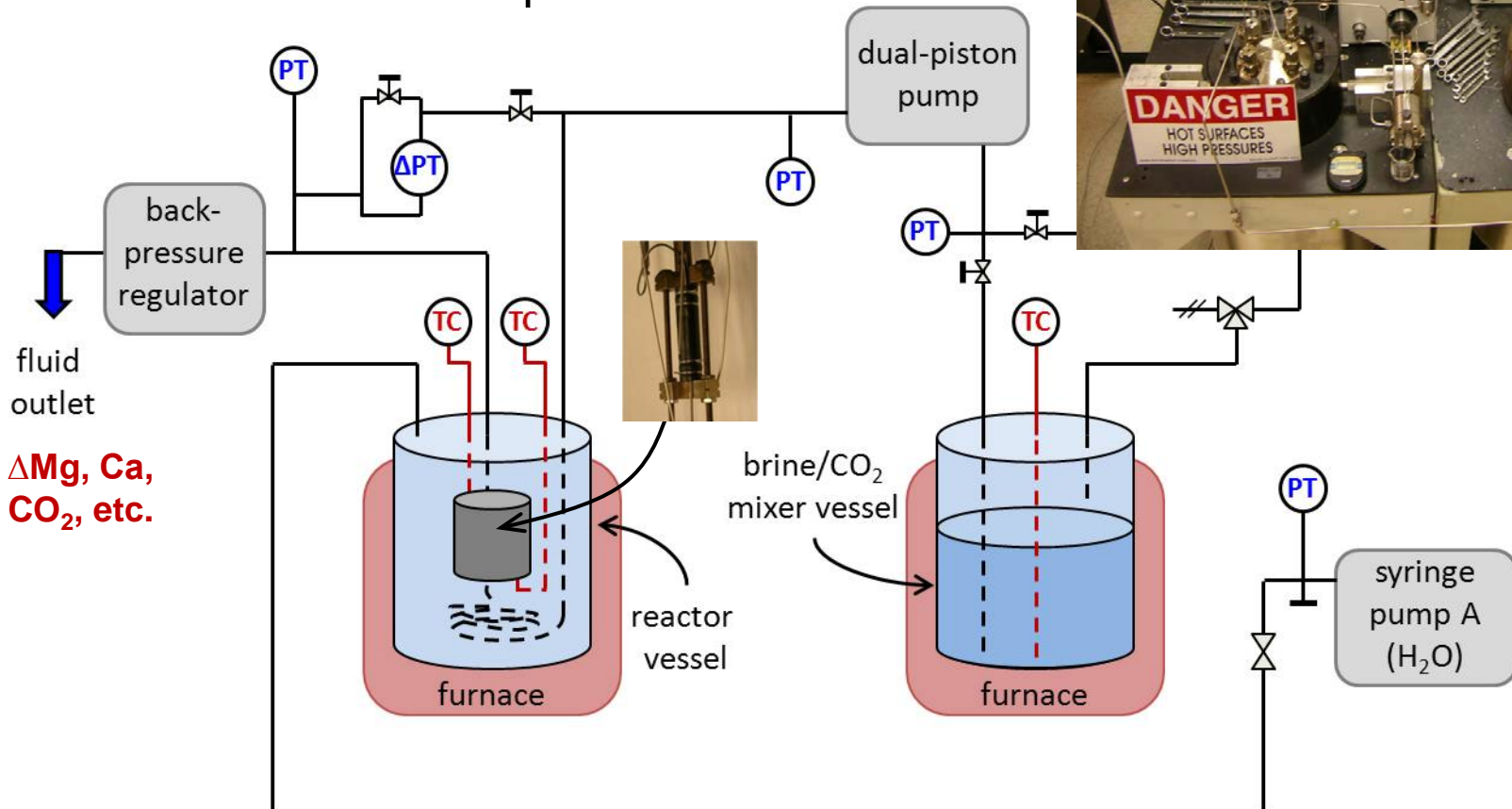
Subcores exhibit lower permeability compared to well log data – larger samples are better



2.5x increase in diameter for “second-generation” Injection zone samples

Core-flood set-up adapted for new KS samples

- 60°C temp, 25 MPa confining pressure
- constant flowrate 0.05 mL/min
- 1.1m NaCl brine with $p\text{CO}_2 = 3 \text{ MPa}$, at carbonate equilibrium



Brine-CO₂ exposure caused little change to properties of Simpson sandstone sample

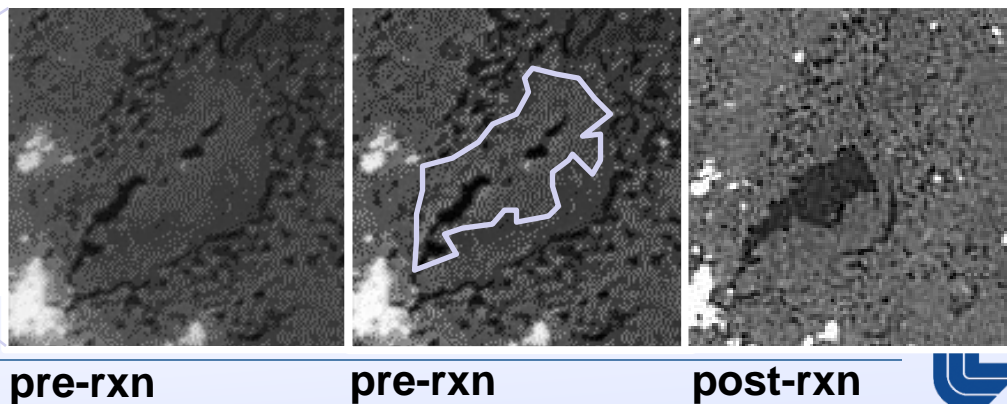
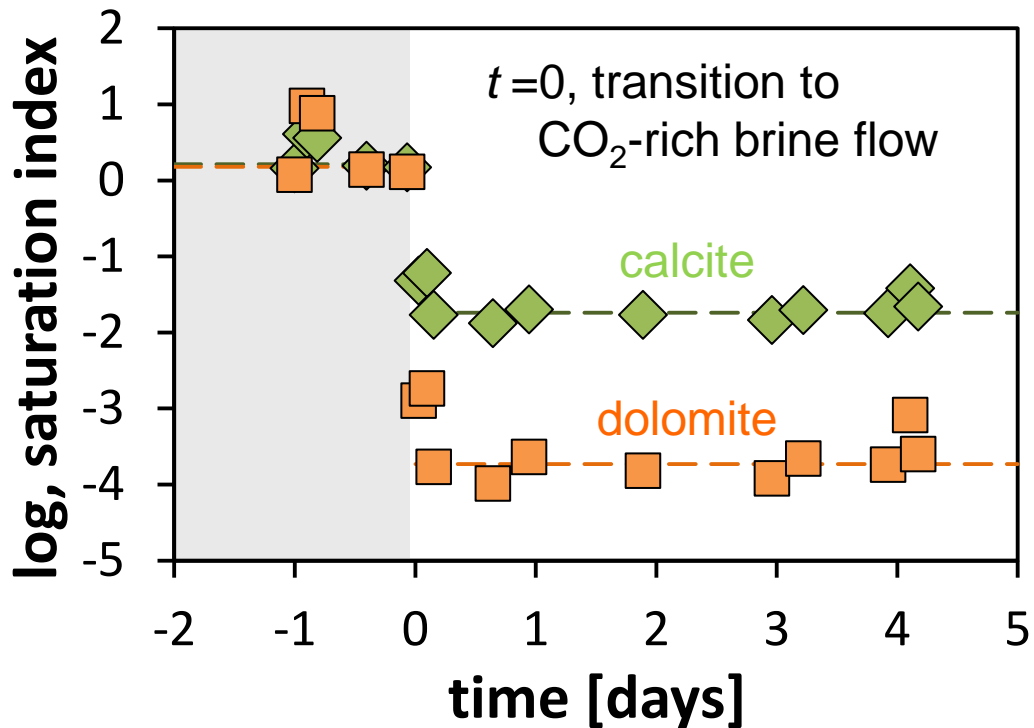
Unreacted Simpson cross-section, (smaller) 15-mm diameter gray-scale tomography image, located ~17mm from inlet

Quartz grains, less cemented

Pyrite grains (bright)

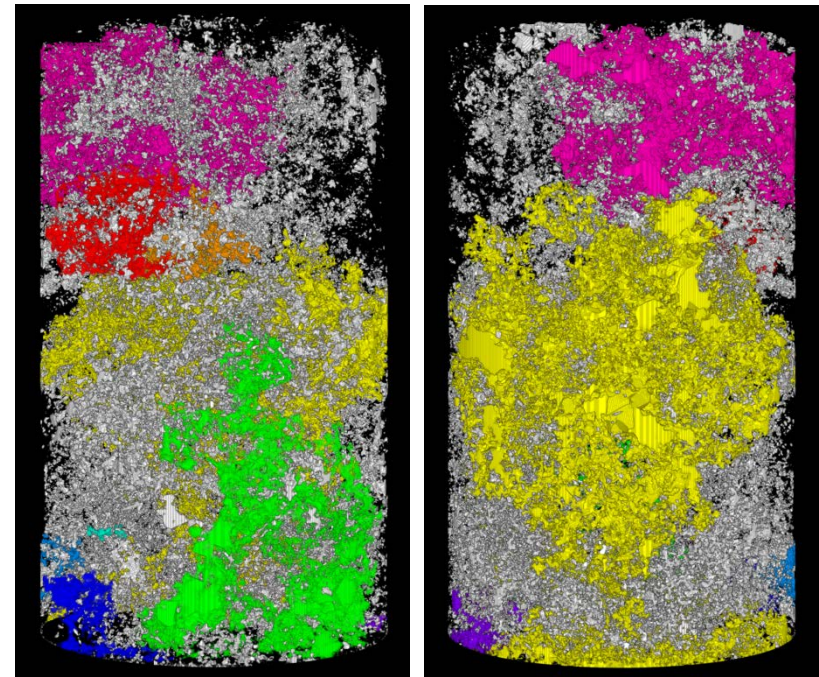
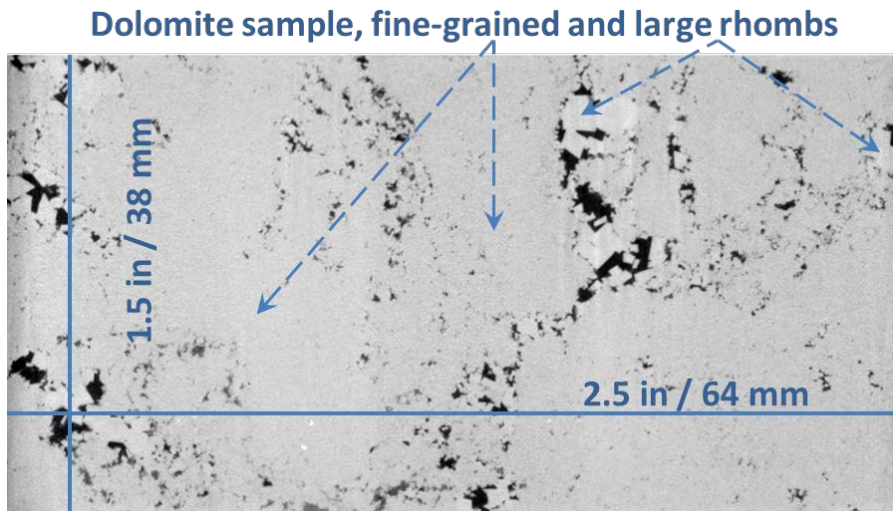
Highly-cemented regions

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Within larger samples, (macro)pore clusters isolated by finer-grained matrix material

Connected macro-pores,
large deep injection zone sample



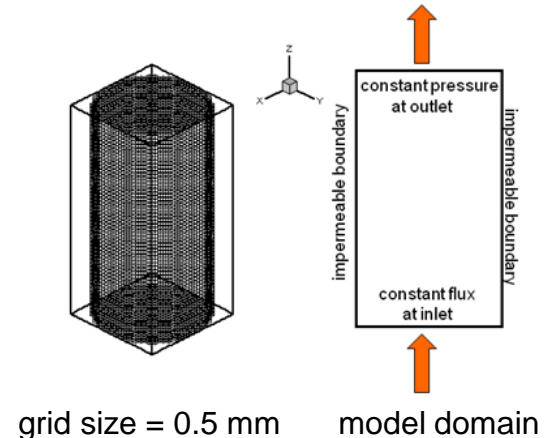
Reactive transport model adaptations for CO₂ core flooding experiments

- ❑ 3-D continuum-scale reactive transport model (NUFT)
- ❑ CO₂-equilibrated brine with pCO₂ = 3 MPa injected into core sample at a constant 0.05 mL/min rate.
 - ❑ Handles either core size (15, 38-mm diameter).
- ❑ Model lateral boundaries kept impermeable; constant pressure and flux conditions imposed at top and bottom boundaries.

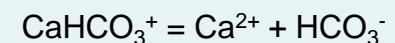
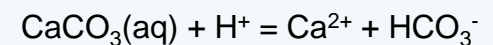
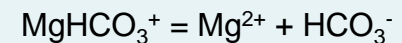
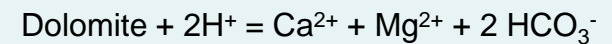
- ❑ Dolomite reaction kinetics

$$\frac{dm}{dt} = -S \left[k_{acid}^{298.15K} e^{-\frac{E_{acid}}{R} \left(\frac{1}{T} - \frac{1}{298.15K} \right)} a_{H^+}^n + k_{neutral}^{298.15K} e^{-\frac{E_{neutral}}{R} \left(\frac{1}{T} - \frac{1}{298.15K} \right)} \right] \left(1 - \frac{Q}{K} \right)$$

- ❑ Utilizes nonlinear porosity–permeability correlation and surface area–porosity relationship



Reactions



Important lessons from previous Weyburn results carried forward in new simulations

- **Chemical Model** – Experiments allow combined reactivity to be calibrated

$$\frac{dm}{dt} = -S \left[k_{acid}^{298.15K} e^{-\frac{E_{acid}}{R} \left(\frac{1}{T} - \frac{1}{298.15K} \right)} a_{H^+}^n + k_{neutral}^{298.15K} e^{-\frac{E_{neutral}}{R} \left(\frac{1}{T} - \frac{1}{298.15K} \right)} \right] \left(1 - \frac{Q}{K} \right)$$

- Rate equations are tied to equilibrium
- Literature equilibrium constants provide starting points
- Calibrations combine rate constants and surface areas
- Pressure changes are not sensitive to reaction rate

- **Porosity – Permeability – Surface Area Relationships**

- Change surface area in proportion to decreasing spherical grains
- “*n*” and permeability contrast terms allow for coupled porosity, permeability evolution

$$S_t = S_0 \left(\frac{\theta_t}{\theta_0} \right)^{2/3} \left(\frac{\phi_t}{\phi_0} \right)^{2/3}$$

$$K_t = K_0 \left(\frac{\phi_t}{\phi_0} \right)^n$$

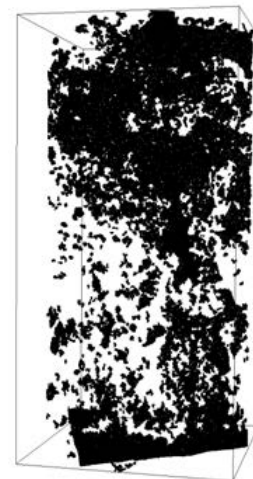
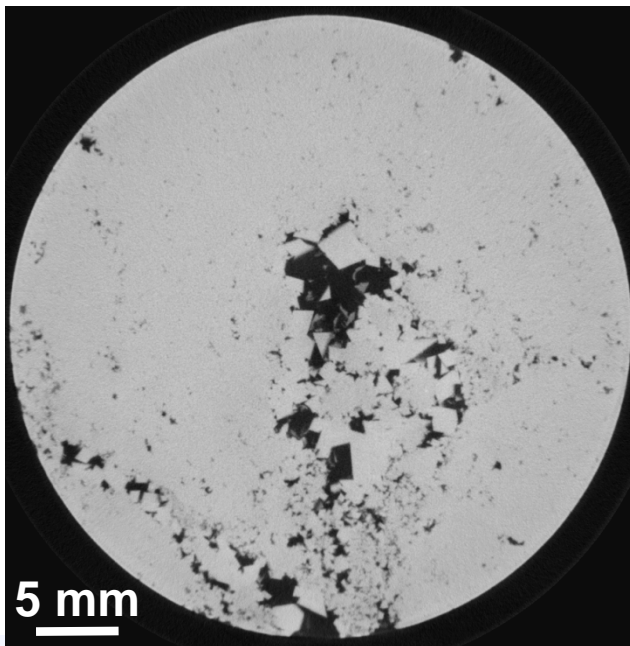


Imaging-based characterization data scaled into larger model grids

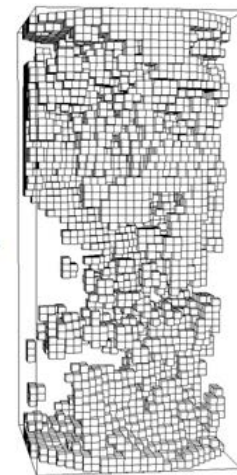
- Effective porosity and mineral phase volume fraction were calculated by a volumetric averaging approach.

$$\phi = \sum_i^N \phi_i / N \quad \theta_m = \sum_i^N \theta_{m,i} / N$$

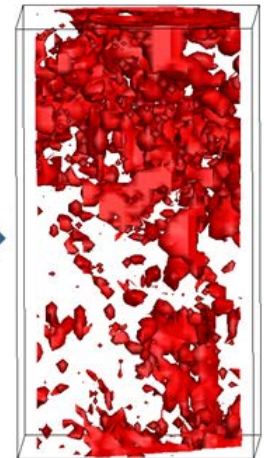
- Permeability distributions were estimated by assessing macro-pore distribution and connectivity. Two porous regions were assumed within the rock sample: one representing interconnected **macro-pore regions**, and the other the **less porous matrix**.



macro-pore connectivity



continuum grid representation



initial model porosity



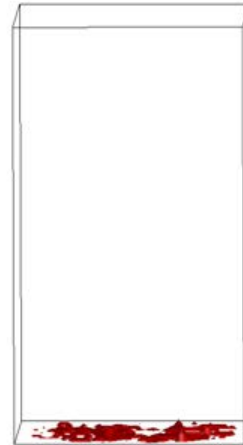
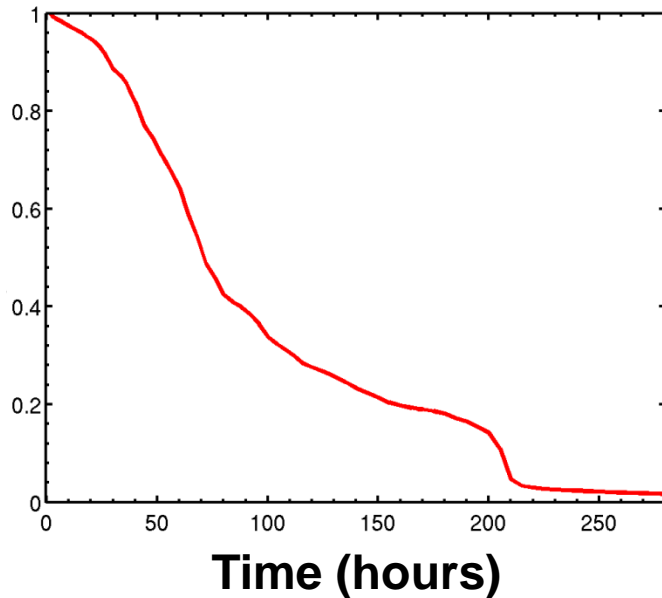
Pre-experiment modeling results — Base Case

- flow rate = **0.05 mL/min**,
porosity-permeability relation $n = 6$,
permeability contrast $K_1/K_2 = 100$,

$$k_{acid}^{298.15K} = 10^{-3.2} \text{ mol/m}^2/\text{s},$$

$$k_{neutral}^{298.15K} = 10^{-7.5} \text{ mol/m}^2/\text{s}.$$

normalized pressure
difference



10 hours



30 hours



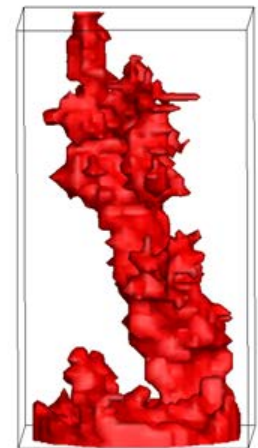
60 hours



120 hours



170 hours

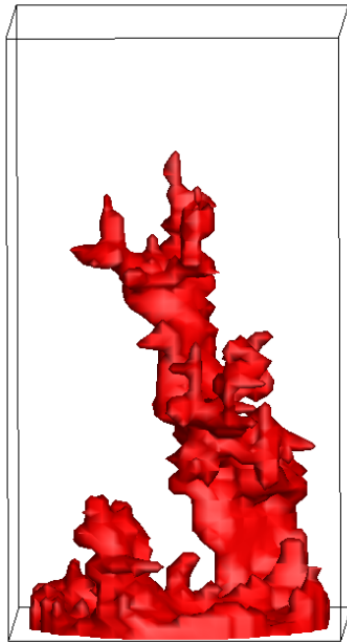


240 hours

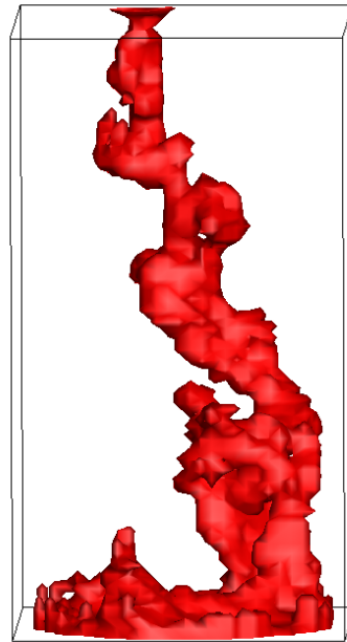


Sensitivity studies — increasing permeability contrast by 10x

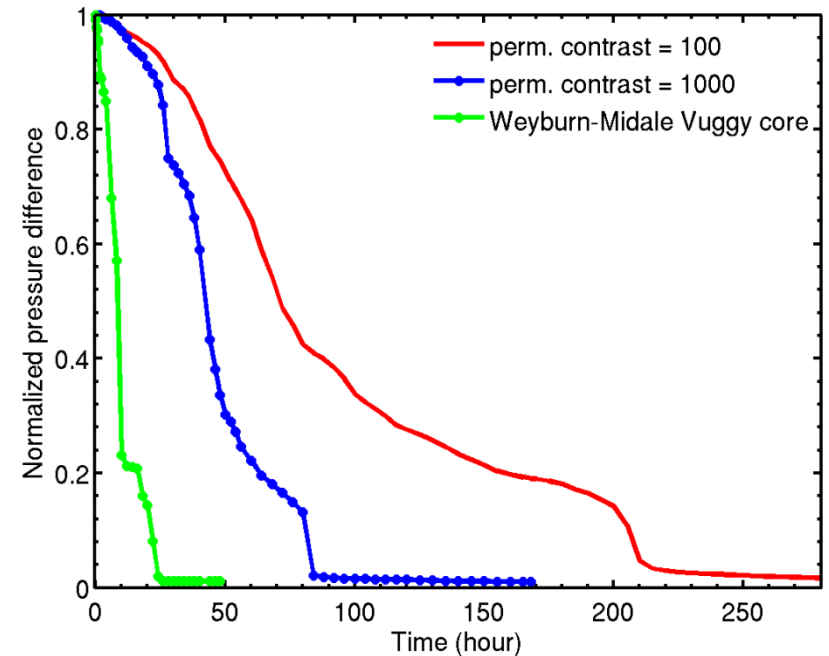
Porosity distributions after CO₂ flooding of **120 hours** (5 days)



low permeability contrast
(base case)

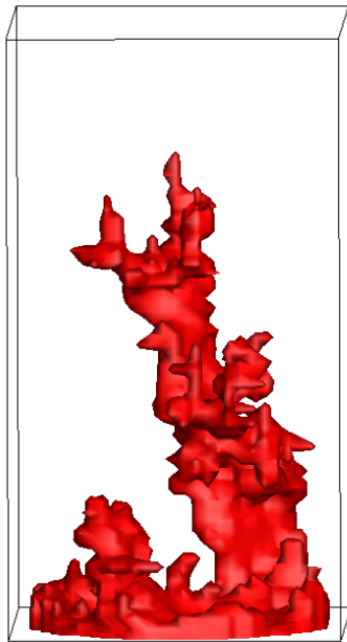


higher
permeability contrast

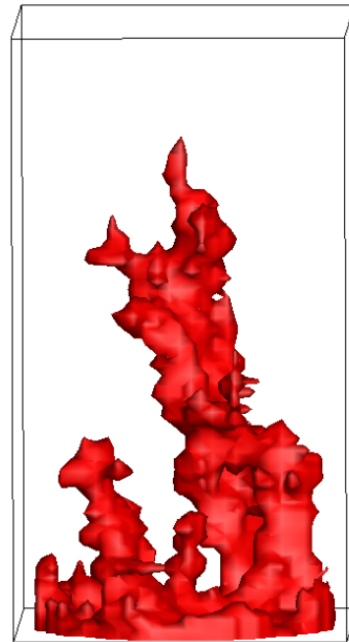


Sensitivity studies — decreasing kinetic constants by 100x (acid) and 10x (neutral mechanism)

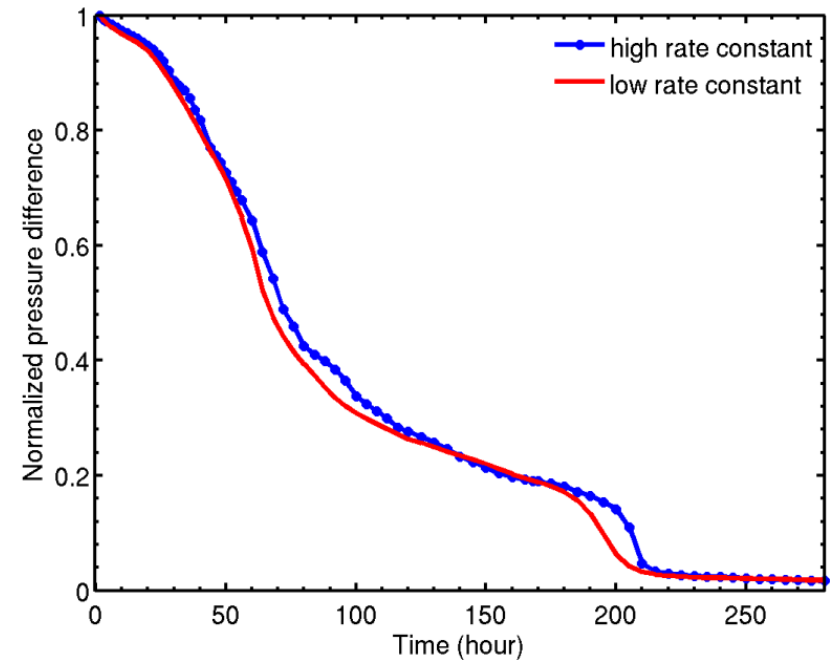
Porosity distributions after CO₂ flooding of **120 hours** (5 days)



high reactivity
(base case)

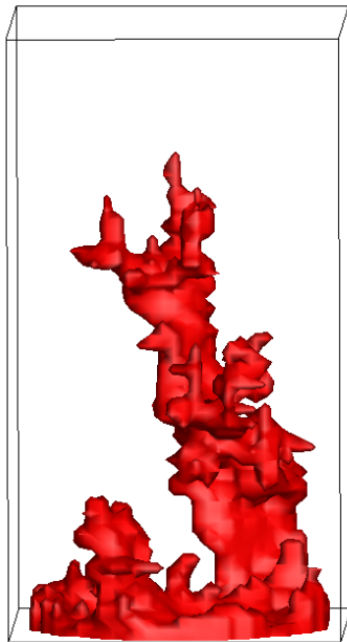


lowered
reactivity

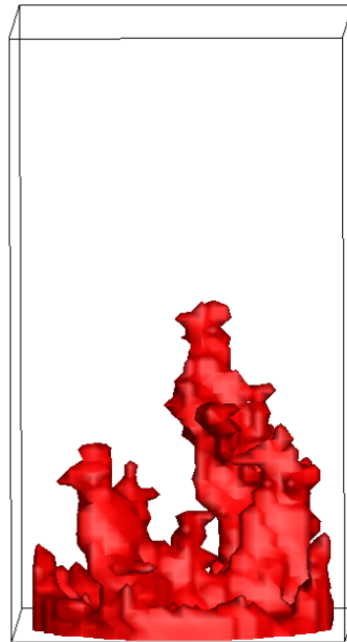


Sensitivity studies — decreasing porosity-permeability relation (n) from 6 to 3

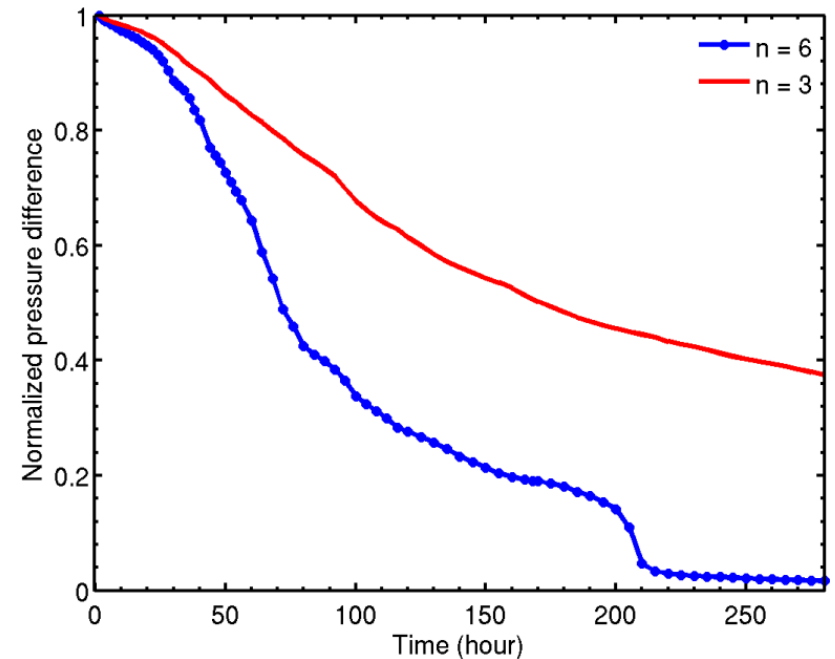
Porosity distributions after CO₂ flooding of **120 hours** (5 days)



$n = 6$
(base case)



$n = 3$



Accomplishments to Date

- ❑ **Publication of results of low permeability caprock response to CO₂ exposure**
(Smith et al., 2012, ES&T)
- ❑ **Weyburn-specific model and scaling results published in special issue**
(Carroll et al., 2013, IJGGC)
- ❑ **Development of model methodology to incorporate varying scales of characterization data to be published** *(Hao et al., in final revision, AWR)*
- ❑ **Additional samples from Arbuckle reservoir (Wellington, KS, KGS) acquired, imaged via CT, and characterized**
- ❑ **One full-length Simpson (Wellington, KS) experiment completed; Results of eight Weyburn experiments to be published** *(Smith et al., in final revision, AWR)*
- ❑ **Equipment modified to accept larger core samples**
(first larger-scale core to be tested September 2013)
- ❑ **Pre-experimental modeling completed to inform upcoming experiments**



Project Summary

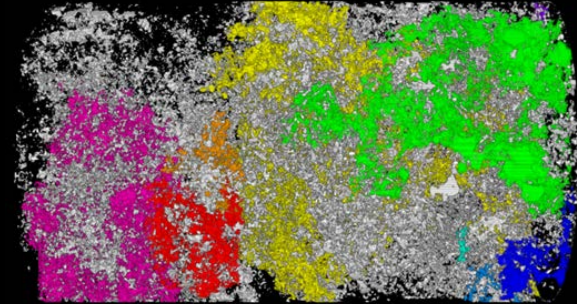
Implications for reservoir scale CCUS simulations

□ Key Findings

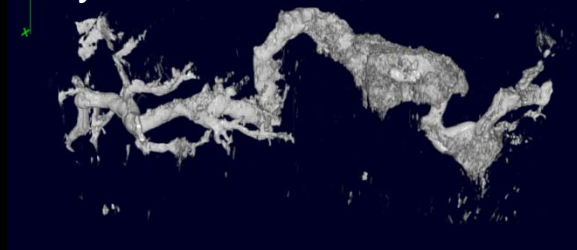
- Anisotropic permeability and mineral dissolution play dominant roles in porosity and permeability changes that will occur during CCUS operations
- Calibrated several reactive transport parameters that scale from microns to centimeters
- Porosity – Permeability relationships are dependent on sample heterogeneity
 - pore regions are not well connected at previous core scales

- ### □ Future Plans:
- Refining the reactive-transport model, calibrating NMR well logs with experiments from the Wellington, KS, CO₂ demonstration site

Wellington, KS, dolomite



Weyburn, Canada, limestone



Weyburn, Canada, dolostone

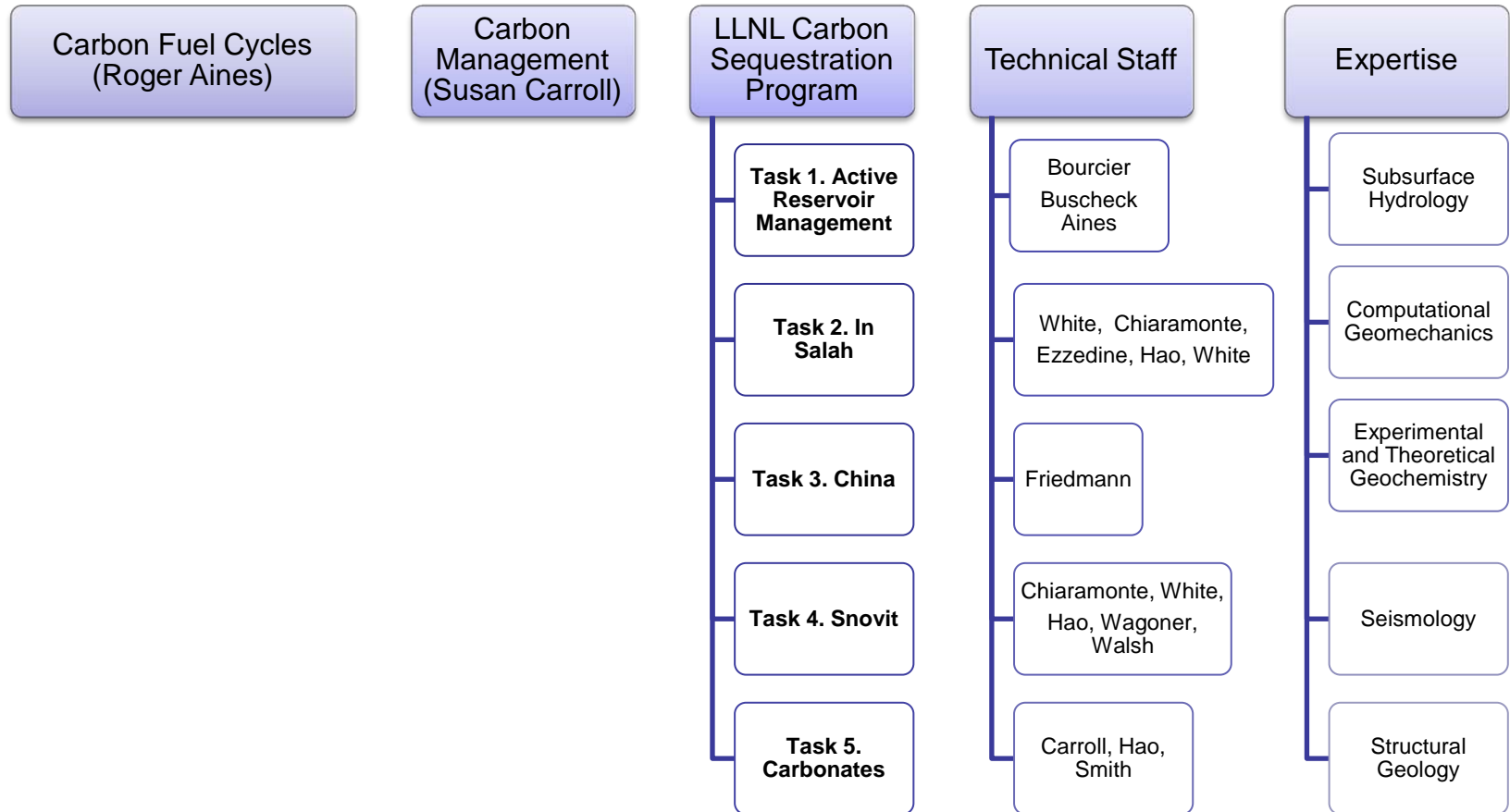


Appendix

- Organizational Chart
- Gantt Chart
- Bibliography



Organization Chart



Gantt Chart: Task 5 Carbonates

		Fiscal Year 2012				Fiscal Year 2013				Fiscal Year 2014			
		Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4
5.1.1	Finish model calibration with Weyburn data	■	■	■	■	■							
5.1.2	Finish premodel simulations for new experiments		■	■	■	■	■						
5.1.3	Refine model using new data						■	■	■	■	■	■	■
5.1.1	Experimental Design	■	■										
5.2.2	Conduct experiments			■	■	■	■	■	■	■	■	■	
5.2.3	Interpret experimental results						■	■	■	■	■	■	



Bibliography

- Smith, M., Sholokhova, Y., Hao Y., and Carroll, S., 2013, Evaporite caprock integrity: An experimental study of reactive mineralogy and pore – scale heterogeneity during brine – CO₂ exposure. Environmental Science and Technology, <http://dx.doi.org/es3012723>.
- Carroll, S. Hao, Y., Smith, M., Sholokhova, Y. (2013), Development of scaling parameters to describe CO₂-carbonate-rock interactions for the Marly Dolostone and Vuggy Limestone, / *J Greenhouse Gas Control*, <http://dx.doi.org/10.1016/j.ijggc.2012.12.026>
- Smith, M. Sholokhova, Y., Hao, Y., and Carroll, S. (2013) CO₂-Induced Dissolution of Low Permeability Carbonates Part I: Characterization and Experiments, Advances in Water Resources, revised.
- Hao, Y., Smith, M., Sholokhova, Y., and Carroll, S. (2013) CO₂-Induced Dissolution of Low Permeability Carbonates Part 2: Numerical Modeling of Experiments, Advances in Water Resources, revised.

